

EXPERIMENTAL COMPARISON OF SINGLE AND MULTISTAGE AIR COMPRESSOR EFFICIENCIES UNDER THE SAME RECEIVER TANK PRESSURE

¹P.V.RAMANA & ²D.RAMBABU

¹Associate professor-Mechanical Engineering Department

²Asst. professor-Mechanical Engineering Department

CVR College of Engineering - Hyderabad (T.S)-India

ABSTRACT

Compressors are widely used for many engineering applications in day to day life. Compressors are classified based on design as reciprocating and rotary compressors, Reciprocating compressors are single acting ,double acting ,air cooled ,water cooled and single stage ,multistage ,depends on application of usage. It is clear by theory as given by author's multistage compressors having advantage over single stage compressors but practically not aware to what extent the variations in efficiencies are taking place and exact experimental figures in that area not focused with clarity. So here focus is given to conduct experiment on both single stage and multi stage compressors at the different receiver tank pressure. Obtained readings are calculated for the same receiver tank pressure and then comparing the results for both the compressors. To know the variations in efficiencies of both compressors results are tabulated and compared to find out the efficiencies for better understanding the subject.

Keywords: single stage compressor, multistage compressor, LP cylinder, HP cylinder, volumetric efficiency, isothermal efficiency.

1.0 INTRODUCTION

Reciprocating air compressors are widely used to get high discharge pressure. To get high discharge pressure single stage compressor has to work against high compression ratio in terms of pressure so to withstand high compression ratio body of compressor also be made robust in construction . It will add more weight to compressor and also leads many mechanical problems because it is working for the development of high pressure in single cylinder and also it is not suitable because of this reasons when to go for developing high delivery pressure for industrial applications. So alternative is increasing the delivery pressure in number of cylinders step by step and reducing the weight of the compressor. first developing pressure in one cylinder of

cylinder say L.P cylinder and allow this pressurized air to another cylinder say Intermediate cylinder (IP) and develop Higher pressure higher than the LP cylinder and allow this pressurized air in another cylinder say HP cylinder and develop more pressure then intermediate cylinder finally highly developed pressurized air is delivered to the end user applications. This is possible by going for multi stage cylinder compressor. This paper focused on conducting the experiment on compressors to find what differences made when using single and multistage compressor in efficiencies and comparing its experimental results for giving the conclusions for the usage.

2.0 EXPERIMENTAL SET UP OF SINGLE STAGE COMPRESSOR

The details of the experimental setup of single stage reciprocating Air compressor is as follows



Fig1: single stage reciprocating Air compressor

Specifications of the compressor:

Make	: ELGI
Type	: Reciprocating Type
Stage	: single stage
Cylinder	: single cylinder
Bore	: 60 mm
Stroke length	: 60 mm
Motor rating	: 2 HP
Motor speed	: 1420 RPM
Compressor speed	: 930 RPM
Electric supply	: 415V/380V, 3ph, 50 HZ
Type of starter	: DOI
Belt size	: B40
Type of lubrication	: splash
Type of cooling	: Air cooled
Type of fan	: forced draught

3.0 SINGLE STAGE COMPRESSOR

Table1: table of Readings of single stage compressor as follows

S . N O	Reciever Tank Pressure (bars)	Suction Pressure P1 (bars)	Discharge pressure P2 (bars)	Suction Temperature T ₁ °C	Discharge Temperature T ₂ °C	Speed RPM	Manometer Reading (mm)	Time per 10 Revolution s-sec
1	2	1	3.8	24	109	876.0	20	6.78
2	4	1	6.4	24	125	872.2	15	6.5
3	6	1	8.4	24	136	869.3	14	6.0

T₁ = suction Temperature of air entering in to the cylinder

T₂ = discharge Temperature of air leaving the compressor

T_a = Ambient Temperature of air

P₁ = suction pressure of air

P₂ = discharge (cylinder outlet) pressure

3.1 Sample calculations for Reading -1 at 2 bar pressure

Sample calculations for Reading -1

Volume of air sucked in to the cylinder

$$V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \quad M^3/hr$$

$$\text{Where } H = \frac{20}{1000} \times \frac{1000}{1.187} = 16.825 \text{ meters}$$

$$V_a = 0.62 \times 1.767 \times 10^{-4} \times \sqrt{2 \times 9.81 \times 16.825} \times 3600 = 7.1656 \quad M^3/hr$$

Theoretical volume of air

$$V_{th} = \frac{\pi}{4} d^2 \times L \times N \times 60 \quad M^3/hr$$

$$V_{th} = \frac{\pi}{4} \times 0.06^2 \times 0.06 \times 876 \times 60 = 8.9165 \quad M^3/hr$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = \frac{7.1656}{8.9165} \times 100 = 80.3\%$$

$$\text{Compression ratio } R_p = \frac{P_2}{P_1} = \frac{3.8}{1} = 3.8$$

$$P_{iso} = \max R \times T_1 \times \ln(R_p)$$

$$\text{Where } m_a = V_a \times \rho_a$$

$$\rho_a = \text{density of air}$$

$$m_a = 7.1656 \times 1.1887 = 8.5117 \quad M^3/hr$$

$$P_{iso} = \max R \times T_1 \times \ln(R_p)$$

$$P_{iso} = \frac{8.5117}{3600} \times 0.287 \times T_1 (273+24) \times \ln(3.8) = 0.269 \text{ KW}$$

As per the relation (temperature, pressure and volume) for polytrophic process $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}}$

$$\ln\left(\frac{273+109}{297}\right) = \frac{n-1}{n} \times \ln(3.8)$$

$$\frac{n-1}{n} = \frac{0.2516}{1.335} = 0.1885$$

$$I.P = \frac{n-1}{n} \times \max RaxT_1 \left[\left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}} - 1 \right]$$

$$I.P = \frac{1}{0.1885} \times \frac{8.5117}{3600} \times 0.287 \times 297$$

$$[(3.8)^{0.1885} - 1] = 0.302 \text{ KW}$$

Power input to Motor (Pm)

$$P_m = \frac{10 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = \frac{10 \text{ rev} \times 3600}{6.78 \times 3200} = 1.659 \text{ KW}$$

$$\text{Power input to compressor } P_c = P_m \times 0.8$$

$$P_c = 1.659 \times 0.8 = 1.327 \text{ Kw}$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = \frac{0.302}{1.327} \times 100 = 22.75 \%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = \frac{0.269}{1.327} \times 100 = 20.27 \%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = \frac{0.269}{0.302} \times 100 = 89 \%$$

3.2 Similarly Sample calculations for Reading -2 at 4 bar pressure

Volume of air sucked in to the cylinder

$$V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \quad M^3/hr$$

Where H = 12.618 meters

$$V_a = 6.256 \quad M^3/hr$$

Theoretical volume of air

$$V_{th} = \frac{\pi}{4} d^2 \times L \times N \times 60 \quad M^3/hr$$

$$V_{th} = 8.877 \quad M^3/hr$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = 70.46\%$$

$$\text{Compression ratio } R_p = \frac{P_2}{P_1} = 6.4$$

$$P_{iso} = \max RaxT_1 \times \ln(R_p)$$

Where $m_a = V_a \times \rho_a$

ρ_a = density of air

$$m_a = 7.4365 \quad M^3/hr$$

$$P_{iso} = \max RaxT_1 \times \ln(R_p)$$

$$P_{iso} = 0.326 \text{ KW}$$

As per the relation (temperature, pressure and volume) for polytrophic process $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}}$

$$\ln\left(\frac{273+125}{297}\right) = \frac{n-1}{n} \times \ln(6.4)$$

$$\frac{n-1}{n} = 0.15768$$

$$I.P = \frac{n-1}{n} \times \max RaxT_1 \left[\left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}} - 1 \right]$$

$$I.P = 0.3796 \text{ KW}$$

Power input to Motor (Pm)

$$P_m = \frac{10 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = 1.7307 \text{ KW}$$

$$\text{Power input to compressor } P_c = P_m \times 0.8$$

$$P_c = 1.7307 \times 0.8$$

$$= 1.384 \text{ Kw}$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = 27.41 \%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = 23.5 \%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = 85.8\%$$

3.3 Similarly Sample calculations for Reading -3 at 6 bar pressure

Volume of air sucked in to the cylinder

$$V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \quad \text{M}^3/\text{hr}$$

Where H = 11.77 meters

$$V_a = 5.995 \quad \text{M}^3/\text{hr}$$

Theoretical volume of air

$$V_{th} = \frac{\pi}{4} d^2 \times L \times N \times 60 \quad \text{M}^3/\text{hr}$$

$$V_{th} = 8.877 \text{ M}^3/\text{hr}$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = 67.52 \%$$

$$\text{Compression ratio } R_p = \frac{P_2}{P_1} = 8.4$$

$$P_{iso} = \max RaxT_1 \times \ln(R_p)$$

Where $m_a = V_a \times \rho_a$

ρ_a = density of air

$$M_a = 7.126 \text{ M}^3/\text{hr}$$

$$P_{iso} = \max RaxT_1 \times \ln(R_p)$$

$$P_{iso} = 0.359 \text{ KW}$$

As per the relation (temperature, pressure and volume) for polytrophic process $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}}$

$$\ln\left(\frac{273+136}{297}\right) = \frac{n-1}{n} \times \ln(8.4)$$

$$\frac{n-1}{n} = 0.1503$$

$$I.P = \frac{n-1}{n} \times \max RaxT_1 \left[\left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}} - 1 \right]$$

$$I.P = 0.423 \text{ KW}$$

Power input to Motor (P_m)

$$P_m = \frac{10 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = 1.875 \text{ KW}$$

Power input to compressor $P_c = P_m \times 0.8$

$$P_c = 1.875 \times 0.8 = 1.5 \text{ Kw}$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = 28.2 \%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = 23.9 \%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = 84.8\%$$

3.4 Comparisons table of values for single stage compressor

Table2: table of results

B a r	η_v ol	P_{is} o	IP	P_c	η_{im} ech	η_o vera ll	η_i so	T 2	R P M
2	80 .3	0. 26 9	0.3 02	1. 32 7	22 .7 5	20 .2 7	8 9. 0	1 0 9	87 6
4	70 .4 6	0. 32 6	0.3 79 6	1. 38 4	27 .4 1	23 .5	8 5. 8	1 2 5	87 2. 2
6	67 .5 2	0. 35 9	0.4 23	1. 5	28 .2	23 .9	8 4. 8	1 3 6	86 9. 3

Comparison shows as pressure is increasing volumetric efficiency and isothermal efficiency is decreasing but isothermal power increases and also other efficiencies like mechanical, overall efficiencies are increases with increase of the pressure

4.0 EXPERIMENTAL SET UP OF MULTISTAGE COMPRESSOR



Fig2: multistage compressor test rig.

Specifications of the compressor:

Make	: ELGI
Model	: TS 03120
Type	: Reciprocating Type
Stage	: two stages
Cylinder	: two cylinders
LP cylinder bore	: 70 mm
HP cylinder bore	: 50 mm

Stroke length	: 85mm
Motor rating	: 3 HP
Motor speed	: 1420 RPM
Compressor speed	: 930 RPM
Electric supply	: 415V/380V, 3ph, 50 HZ
Type of starter	: DOI
Belt size	: A68
Type of lubrication	: splash
Type of cooling	: Air cooled
Type of fan	: forced draught

5.0 MULTISTAGE COMPRESSOR

Table3: Table of Readings of multistage compressor as follows

Ta nk Pr ess ur e	P 1	P 2	P 3	M a n o m e t er	Time per 5 revol ution s	RPM	T 1	T 2	T 3	T 4
2	1	0 .9 5	1 .9 0	2 0 0	42.75	928	2 8	1 0 0	8 6	8 8
4	1	1 .0 5	4 .4 5	1 9 3	36.97	923	2 9	1 1 4	9 6	1 3 1
6	1	1 .1 4	6 .1 9	1 8 9	34.59	917	2 9	1 1 4	9 8	1 5 7

T_1 =Temperature of air entering L.P cylinder
 T_2 =Temperature of air leaving L.P cylinder
 T_3 =Temperature of air after intercooler and entering H.P cylinder
 T_4 = temperature air leaving HP cylinder
 T_a = ambient temperature/
 P_1 = atmosphere pressure 1 bar
 P_2 = L.P cylinder outlet pressure
 P_3 = H.P cylinder outlet pressure

5.1 Sample calculations for Reading -1 at 2 bar pressure

Sample calculations for Reading -1

Volume of air sucked in to the cylinder
 $V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \quad M^3/hr$

$$\text{Where } H = \frac{200}{1000} \times \frac{1000}{1.1729} = 170.517 \text{ meters}$$

$$V_a = 0.62 \times 1.767 \times 10^{-4} \times \sqrt{2 \times 9.81 \times 170516} \times 3600 = 22.812 \text{ M}^3/\text{hr}$$

Theoretical volume of air

$$V_{th} = L \times N_c (A_1 + A_2) \times 60 \text{ M}^3/\text{hr}$$

$$\text{Area of first cylinder-} A_1 = \frac{\pi}{4} d_1^2$$

$$\text{Area of first cylinder-} A_1 = \frac{\pi}{4} d_2^2$$

$$V_{th} = 0.085 \times 928 (1.9634 \times 10^{-3} + 3.848 \times 10^{-3}) \times 60 \text{ M}^3/\text{hr}$$

$$V_{th} = 27.506 \text{ M}^3/\text{hr}$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = \frac{22.812}{27.506} \times 100 = 82.9\%$$

$$\text{Compression ratio } R_p = \frac{P_3}{P_1} = \frac{1.9}{1} = 1.9$$

$$P_{iso} = \max R_a x T_1 \times \ln(R_p)$$

$$\text{Where } m_a = V_a \times \rho_a$$

$$\rho_a = \text{density of air}$$

$$\rho_a = \text{density of air} = \frac{101.325}{0.287 \times 301} = 1.1729$$

$$m_a = 22.812 \times 1.1729 = 26.756 \text{ M}^3/\text{hr}$$

$$P_{iso} = \max R_a x T_1 \times \ln(R_p)$$

$$P_{iso} = \frac{26.756}{3600} \times 0.287 \times (273+28) \times \ln(1.9) = 0.4121 \text{ KW}$$

As per the relation (temperature, pressure and

$$\text{volume) for polytropic process } \frac{T_4}{T_1} = \left(\frac{P_3}{P_1}\right)^{\frac{n-1}{n}}$$

$$\ln\left(\frac{273+88}{273+28}\right) = \frac{n-1}{n} \times \ln(1.9)$$

$$\frac{n-1}{n} = \frac{0.18176}{0.641} = 0.28317 \text{ and } n = 1.396$$

$$I.P = 2x \frac{n-1}{n} \times \max R_a x T_1 \left[\left(\frac{P_3}{P_1}\right)^{\frac{n-1}{2n}} - 1\right]$$

$$I.P = \frac{2}{0.283179} \times \frac{26.756}{3600} \times 0.287 \times 301 \left[(1.9)^{\frac{1.396-1}{2 \times 1.396}} - 1\right] = 0.430 \text{ KW}$$

Power input to Motor (Pm)

$$P_m = \frac{5 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = \frac{5 \text{ rev} \times 3600}{42.75 \times 3200} = 2.105 \text{ KW}$$

$$\text{Power input to compressor } P_c = P_m \times 0.8$$

$$P_c = 2.105 \times 0.8 =$$

$$1.684 \text{ Kw}$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = \frac{0.430}{1.684} \times 100 =$$

$$25.53\%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = \frac{0.4121}{1.684} \times 100$$

$$= 24.47 \%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = \frac{0.4121}{0.430} \times 100 =$$

$$95.9 \%$$

5.2 Sample calculations for Reading -2 at 4 bar pressure

Sample calculations for Reading -2

Volume of air sucked in to the cylinder

$$V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \text{ M}^3/\text{hr}$$

$$\text{Where } H = 164.549 \text{ meters}$$

$$V_a = 0.62 \times 1.767 \times 10^{-4} \times \sqrt{2 \times 9.81 \times 170516} \times 3600 = 22.812 \text{ M}^3/\text{hr}$$

Theoretical volume of air

$$V_{th} = L \times N_c (A_1 + A_2) \times 60 \quad M^3/hr$$

$$\text{Area of first cylinder}-A_1 = \frac{\pi}{4} d_1^2$$

$$\text{Area of first cylinder}-A_1 = \frac{\pi}{4} d_2^2$$

$$V_{th} = 0.085 \times 923 (1.9634 \times 10^{-3} + 3.848 \times 10^{-3}) \times 60 \quad M^3/hr$$

$$V_{th} = 27.354 \quad M^3/hr$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = \frac{22.409}{27.345} \times 100 = 81.9\%$$

$$\text{Compression ratio } R_p = \frac{P_3}{P_1} = 4.45$$

$$P_{iso} = m_a \times R \times T_1 \times \ln(R_p)$$

Where $m_a = V_a \times \rho_a$

ρ_a = density of air

$$\rho_a = \text{density of air} = \frac{101.325}{0.287 \times 301} = 1.1729$$

$$m_a = 22.409 \times 1.1729 = 26.283 \quad M^3/hr$$

$$P_{iso} = m_a \times R \times T_1 \times \ln(R_p)$$

$$P_{iso} = \frac{26.756}{3600} \times 0.287 \times (273+28) \times \ln(4.45) = 0.9415 \quad KW$$

As per the relation (temperature, pressure and

volume) for polytropic process $\frac{T_4}{T_1} = \left(\frac{P_3}{P_1}\right)^{\frac{n-1}{n}}$

$$\ln\left(\frac{273+131}{273+28}\right) = \frac{n-1}{n} \times \ln(4.45)$$

$$\frac{n-1}{n} = \frac{0.18176}{0.641} = 0.1971 \quad \text{and} \quad n = 1.2454$$

$$I.P = 2x \left(\frac{n-1}{n}\right) \times m_a \times R \times T_1 \left[\left(\frac{P_3}{P_1}\right)^{\frac{n-1}{2n}} - 1\right]$$

$$I.P = 1.0143 \quad KW$$

Power input to Motor (Pm)

$$P_m = \frac{5 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = 2.434 \quad KW$$

Power input to compressor $P_c = P_m \times 0.8$

$$P_c = 2.434 \times 0.8 = 1.947 \quad Kw$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = \frac{1.0143}{1.947} \times 100 = 52.09\%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = \frac{0.9415}{1.947} \times 100 = 48.3 \%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = \frac{0.9415}{1.0143} \times 100 = 92.8 \%$$

5.3 Sample calculations for Reading -3 at 6 bar pressure

Sample calculations for Reading -1

Volume of air sucked in to the cylinder

$$V_a = C_d \times A_o \times \sqrt{2gH} \times 3600 \quad M^3/hr$$

Where H = 161.139 meters

$$V_a = 22.175 \quad M^3/hr$$

Theoretical volume of air

$$V_{th} = L \times N_c (A_1 + A_2) \times 60 \quad M^3/hr$$

$$\text{Area of first cylinder}-A_1 = \frac{\pi}{4} d_1^2$$

$$\text{Area of first cylinder}-A_1 = \frac{\pi}{4} d_2^2$$

$$V_{th} = 0.085 \times 917 (1.9634 \times 10^{-3} + 3.848 \times 10^{-3}) \times 60 \quad M^3/hr$$

$$V_{th} = 27.178 \quad M^3/hr$$

Volumetric efficiency

$$\eta_{vol} = \frac{V_a}{V_{th}} \times 100$$

$$\eta_{vol} = 81.59\%$$

$$\text{Compression ratio } R_p = \frac{P_3}{P_1} = 6.4$$

$$P_{iso} = \max R_a x T_1 \times \ln(R_p)$$

Where $m_a = V_a \times \rho_a$

ρ_a = density of air

$$\rho_a = \text{density of air} = \frac{101.325}{0.287 \times 301} = 1.1729$$

$$m_a = 22.175 \times 1.729 = 26.009 \text{ M}^3/\text{hr}$$

$$P_{iso} = \max R_a x T_1 \times \ln(R_p)$$

$$P_{iso} = \frac{26.009}{3600} \times 0.287 \times (273+28) \times \ln(6.4) = 1.1585 \text{ KW}$$

As per the relation (temperature, pressure and volume) for polytropic process $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}}$

$$\ln\left(\frac{273+157}{273+28}\right) = \frac{n-1}{n} \times \ln(6.4)$$

$$\frac{n-1}{n} = 0.1921 \text{ and } n = 1.2377$$

$$I.P = 2x \frac{n-1}{n} \times \max R_a x T_1 \left[\left(\frac{P_2}{P_1}\right)^{\frac{n-1}{2n}} - 1 \right]$$

$$I.P = 1.2377 \text{ KW}$$

Power input to Motor (Pm)

$$P_m = \frac{5 \text{ rev} \times 3600}{t \text{ in sec} \times 3200}$$

Where 3200 = Energy meter constant

$$P_m = 2.6019 \text{ KW}$$

Power input to compressor $P_c = P_m \times 0.8$

$$P_c = 2.6019 \times 0.8 = 2.0815 \text{ Kw}$$

$$\text{Mechanical efficiency } \eta = \frac{I.P}{P_c} \times 100$$

$$\eta = 59.6\%$$

$$\text{Overall efficiency } \eta = \frac{P_{iso}}{P_c} \times 100$$

$$\eta = 55.6\%$$

$$\text{Isothermal efficiency } \eta = \frac{P_{iso}}{I.P} \times 100$$

$$\eta = 93.5\%$$

5.4 Comparisons of values for multi stage compressor

Table 4: table of results for multistage compressor

pre ssu re	η_v ol	P_{is} o	IP	P_c	η me ch	η_o vr	η_i so	T 4	R P M
2	8 2. 9	0. 41 21	0. 45 19	1. 68 4	2 6. 8	2 4. 4 7	9 1. 1	8 9 8	9 2 8
4	8 1. 9 2	0. 94 15	1. 09 4	1. 94 7	5 6. 1	4 8. 3	8 6. 0 6	1 3 1	9 2 3
6	8 1. 5 9	1. 15 85	1. 33 7	2. 08 15	6 4. 2 3	5 5. 6	8 6. 6	1 5 7	9 1 7

Comparison shows as pressure is increasing volumetric efficiency and isothermal efficiency is decreasing but isothermal power and indicated power increases and also other efficiencies like mechanical, overall efficiencies increases with increase of the pressure. It was observed this is same in both cases of single and multi stage compressor

5.5 Comparisons tables for single stage and multi stage compressors

Table: 5 -Comparisons table for single and multi stage compressor

Tank Pressure	Volumetric Efficiency		P_{iso}		IP	
	Single stage	Multi stage	Single stage	Multi stage	Single stage	Multi stage
2	80.3	82.9	0.209	0.4121	0.302	0.451
4	70.46	81.92	0.326	0.9415	0.3796	1.094
6	67.52	81.59	0.359	1.1585	0.423	1.337

Table: 6 -Comparisons table for single and multistage compressor

Tank Pressure	P_c		η_{mech}		η_{over}	
	Single stage	Multi stage	Single stage	Multi stage	Single stage	Multi stage
2	1.327	1.684	22.75	26.8	20.27	24.47
4	1.384	1.947	27.41	56.1	23.5	48.3
6	1.5	2.0815	28.2	64.23	23.9	55.6

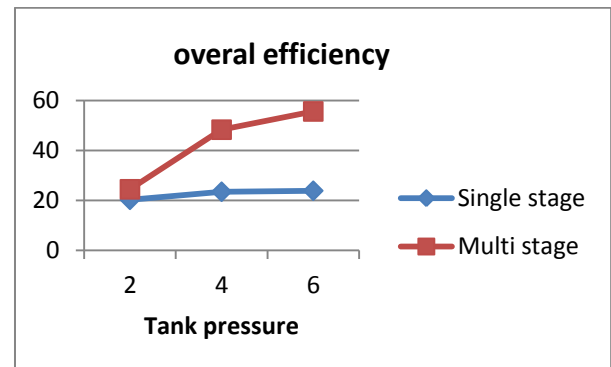
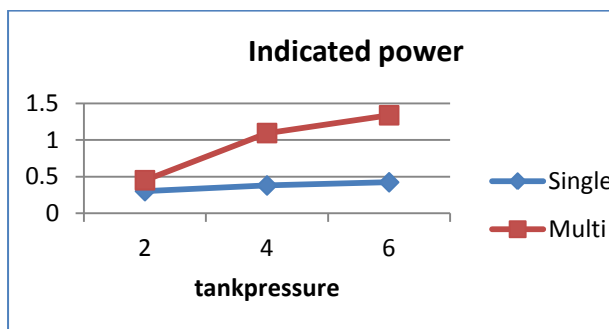
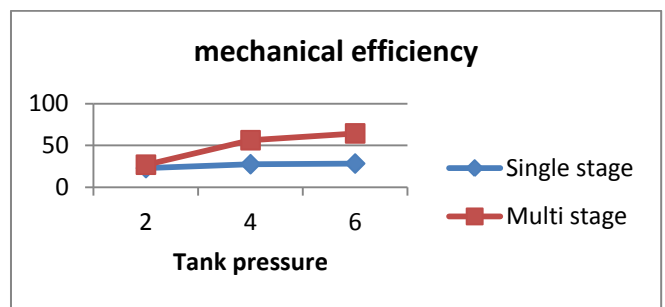
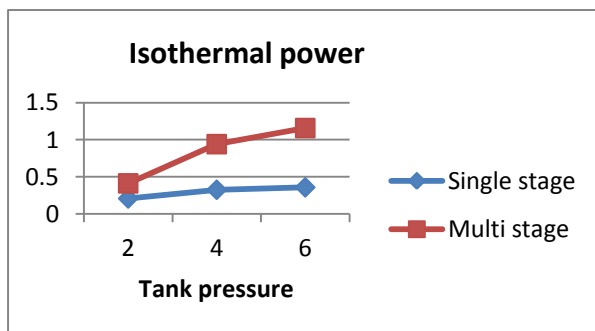
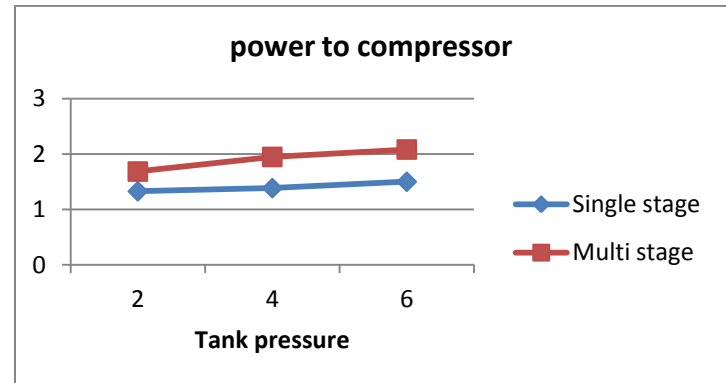
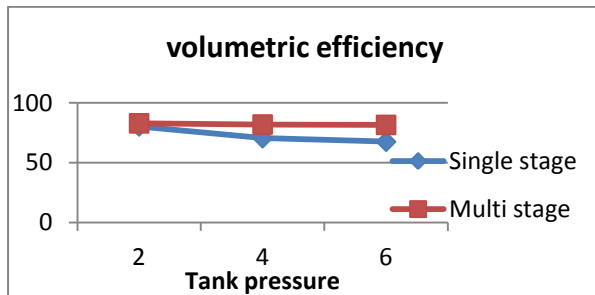


Table: 7 -Comparisons table for single and multi stage compressor

Tank Pressure	η_{iso}		Delivery temperature		RPM	
	Single stage	Multi stage	Single stage	Multi stage	Single stage	Multi stage
2	89.0	91.1	109	88	876	928
4	85.8	86.06	125	131	872.2	923
6	84.8	86.6	136	157	869.3	917

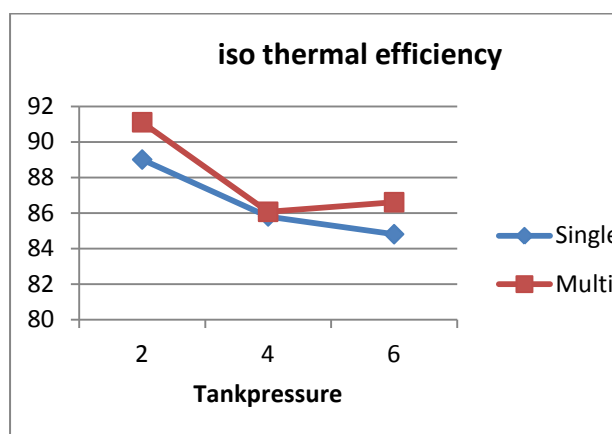
multistage compressor having higher efficiency then the single stage compressor.

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6.0 CONCLUSIONS

It was observed with increase of tank pressure isothermal power, indicated power mechanical efficiencies are increasing for both single and multistage compressors and also observed with increase of delivery pressure volumetric efficiency is reducing in both cases. As temperature of incoming air increasing, the density of air decreasing and volume of air sucked in to cylinder increases, it may be the reason because of less dense of air which may be entering in to the engine cylinder. On comparison of volumetric efficiency, isothermal power indicated power, mechanical efficiency; isothermal efficiencies are higher for multistage compressor then the single stage compressor with marginal rise of power input to the compressor. We may conclude for almost same equal power consumption